



# Low Noise-Wideband Chopper Stabilized Amplifier

## MODEL 234

### PRELIMINARY TECHNICAL DATA

#### FEATURES

Low Drift:  $0.1\mu\text{V}/^\circ\text{C}$ ,  $1\text{pA}/^\circ\text{C}$   
Offset Stability:  $2\mu\text{V}$  per month  
Submicrovolt Noise:  $0.7\mu\text{V}$  p-p (0.01 to 1Hz B.W.)  
Fast Response: 2.5MHz B.W.,  $4\mu\text{sec}$  settling (0.01%)  
Low Cost Module: \$54 (1 to 9),  $1\frac{1}{2}'' \times 1\frac{1}{2}'' \times 0.4''$

#### APPLICATIONS

Precision Wideband Amplification  
Current and Voltage Summation  
High Speed Integration  
Reference Buffering  
Controlled Current Source  
Bridge Amplifier

#### GENERAL DESCRIPTION

Analog Devices' Model 234 is a high performance chopper stabilized op amp which significantly improves on the noise and bandwidth performance of previous designs. Available with drift of  $0.1\mu\text{V}/^\circ\text{C}$ , the Model 234 features  $0.7\mu\text{V}$  p-p input noise and 2.5MHz unity gain bandwidth to satisfy many demanding requirements for a premium amplifier at less than premium prices.

Incorporating MOSFET choppers and discrete components (vs. IC op amps) for the main and stabilizing amplifier channels, this inverting design is virtually free of input chopper spikes and offers reduced modulation ripple for quieter wideband performance. These characteristics are especially desirable when operating from high source impedances (above  $100\text{k}\Omega$ ) at wide bandwidths. To illustrate the improvements in noise and bandwidth performance, over previous Analog Devices' designs, comparative data is set forth in the following sections comparing models 232 and 233 with 234.

Other Model 234 specifications include: gains of  $10^7$  V/V,  $4\mu\text{sec}$  settling time to 0.01% ( $20\text{k}\Omega$  load, 10V) and three selections for voltage drift:  $1\mu\text{V}/^\circ\text{C}$  (234J),  $0.3\mu\text{V}/^\circ\text{C}$  (234K), and  $0.1\mu\text{V}/^\circ\text{C}$  (234L). Available in a compact plug-in module ( $1\frac{1}{2}'' \times 1\frac{1}{2}'' \times 0.4''$ ), Model 234 is competitively priced for new OEM designs and is recommended as a pin compatible replacement for upgrading the performance of most existing designs. The use of premium discrete components throughout assures repeatable unit-to-unit performance for best results at lower costs.

#### APPLICATIONS

In general, the Model 234 inverting amplifier should be considered where long term stability of offset voltage must be



maintained with time and temperature for precision designs, or wherever carefree operation of instruments and remote circuits is essential. Typical applications include low drift amplification of wideband microvolt signals, integration of low duty-cycle pulse trains and fast analog computing for general purpose designs. Low input noise and stable offset voltages also make Model 234 an ideal preamp for precision low frequency applications such as DVM's, 12 to 16 bit A to D converters, and for error amplifiers in servo and null detector systems.

#### IMPROVED NOISE AND BANDWIDTH PERFORMANCE

The improved performance of Model 234 accrues from the use of discrete components throughout, coupled with low noise front-end circuits, all carefully packaged and shielded to minimize pickup and intermodulation effects. Chopper modulation ripple, as shown in Figure 1, is significantly reduced over an earlier design, Model 232, for most wideband applications.

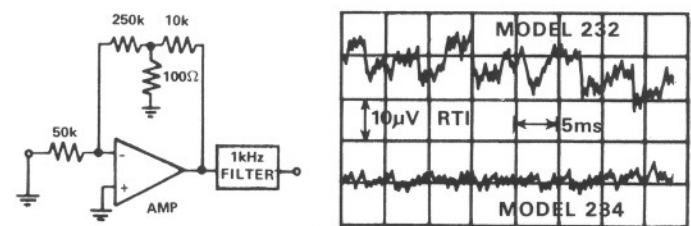


Figure 1. Comparative Input Noise (RTI)  
Performance in a DC to 1kHz Bandwidth.

(continued on page 3)

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# SPECIFICATIONS

(typical @ +25°C and ±15V unless otherwise noted)

MODEL	234J	234K	234L
OPEN LOOP GAIN			
DC, 2k ohm load	10 <sup>7</sup> V/V min	*	*
RATED OUTPUT			
Voltage	±10V min	*	*
Current	±5mA min	*	*
Load Capacitance Range	0-1000pF min	*	*
FREQUENCY			
Unity Gain, Small Signal	2.5MHz	*	*
Full Power Response	500kHz min	*	*
Slew Rate	30V/μsec	*	*
SETTLING TIME to 0.01%			
20kΩ load, 10V step (Figure 2)	4μsec	*	*
INPUT OFFSET VOLTAGE			
Initial Offset, max	±50μV	±20μV	±20μV
vs. Temp, 0°C to +70°C, max	±1.0μV/°C	±0.3μV/°C	±0.1μV/°C
vs. Supply Voltage	±0.2μV/%	*	*
vs. Time	±2μV/month	*	*
vs. Turn On, 10 sec to 10 min	±3μV	*	*
INPUT BIAS CURRENT			
Initial, max	±100pA	*	*
vs. Temp, 0°C to +70°C, max	±4pA/°C	±2pA/°C	±1pA/°C
vs. Supply Voltage	±0.5pA/%	*	*
INPUT IMPEDANCE			
Inverting Input to Signal Ground	300k ohms	*	*
INPUT NOISE			
Voltage, 0.01 to 1Hz	0.7μV p-p	*	*
0.1 to 10Hz	1.5μV p-p	*	*
10Hz to 10kHz	2μV rms	*	*
Current, 0.01 to 1Hz	2pA p-p	*	*
0.1 to 10Hz	4pA p-p	*	*
INPUT VOLTAGE RANGE			
(-) Input to Signal Ground	±15V max	*	*
POWER SUPPLY (VDC)			
Rated Performance	±15V @ 5mA	*	*
Operating	±(12 to 18)V	*	*
TEMPERATURE RANGE			
Rated Specifications <sup>1</sup>	0°C to +70°C	*	*
Operating	-25°C to +85°C	*	*
Storage	-25°C to +100°C	*	*
PRICE			
(1-9)	\$54.	\$65.	\$89.
(10-24)	\$49.	\$59.	\$82.

\*Specifications same as Model 234J.

<sup>1</sup> Models 234A and 234B meet rated specifications of Models 234J and 234K over range of -25°C to +85°C. Contact Factory or Sales Office for price and delivery. Specifications subject to change without notice.

## OPEN LOOP GAIN AND PHASE SHIFT

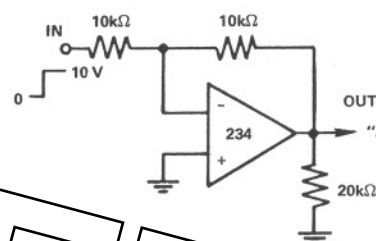
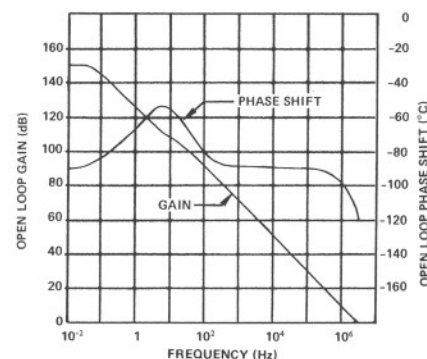
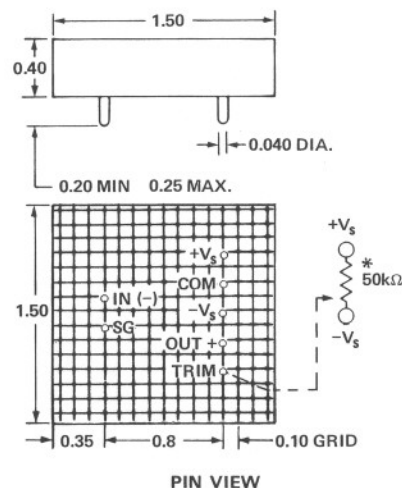


Figure 2. Settling Time Test Circuit Using Scope Comparator Preamp at "A"

## OUTLINE DIMENSIONS (In Inches)



### NOTES:

\*Optional Trim Pot Analog Devices Model 79PR50k [\$3.00 ea. (1-9)] Connect Trim Terminal to Common if Trim Pot is not used.

1. SG Tied to Common.
2. Mating Socket AC 1010 @ \$3.00.
3. Weight: 27 grams.

# Applying the Chopper Stabilized Amplifier

(continued from page 1)

Shown below are plots of typical input voltage and input current noise over the frequency range of 0.01Hz to 10Hz. Particular care has been exercised in the design of this amplifier to reduce the noise level to that commensurate with the low drift performance obtained by chopper stabilization.

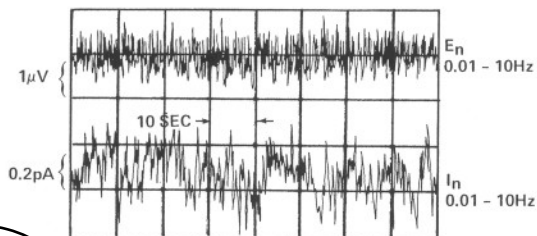


Figure 3. Model 234 Voltage and Current Noise

## INPUT IMPEDANCE CONSIDERATIONS

The maximum input impedance for inverting amplifiers of all types is limited by bias current, bias current drift, and noise current. These currents flowing through the source impedance will increase the total error and noise when the input impedance exceeds  $E/I$ , where  $E$  is a given type of voltage error and  $I$  is the corresponding current error. Figure 4 is a plot of total offset voltage, total voltage drift and total noise vs. input resistance for the Model 234. Up to 100,000 ohms, the Model 234 provides relatively constant levels of offset, noise, and drift. Above this resistance level, the bias current effects become more predominant.

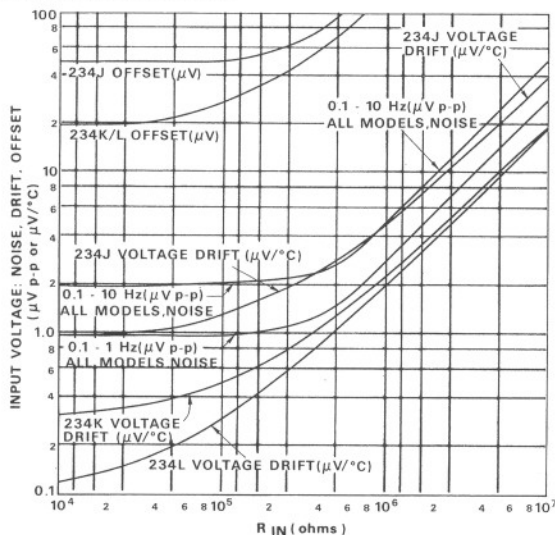


Figure 4. Uncompensated Offset, Drift and Noise vs.  $R_{in}$

## INITIAL OFFSET ADJUSTMENT

A valuable characteristic of the Model 234 is the low offset voltage without external trim. The specification is 50μV maximum for the Model 234J, and 20μV maximum for the Models 234K and 234L. In many applications there will be no need to zero the offset since it is so low. In such cases the trim terminal may either be left open, or grounded, whichever is more convenient for the user. If voltage offset adjustment is desired, it may be done with a potentiometer or selected fixed resistor network, as shown in the outline drawing on page 2.

Input bias current flowing through the input resistor(s) creates additional voltage offset, particularly with input resistances exceeding 500,000 ohms. For circuits where the total input and source resistance remain relatively constant, the entire offset may be zeroed out with the voltage offset adjustment. No additional drift will occur with the Model 234 when voltage trimming is used to compensate for the offset effects of input bias current.

The circuit of Figure 5 should be used to compensate for bias current offsets when using the Model 234 as a current to voltage converter. The potentiometer-resistor network provides a compensating bias current to cancel the amplifier's own input bias current. The offset voltage trim may be used but is not necessary when using this technique.

When the amplifier is used with a widely varying input resistance and minimum offset is desired, the voltage and current trim potentiometers should be used. The voltage offset should be zeroed with a low value (e.g. 1k ohm) resistor connected from the inverting input to ground. The offset current adjustment should be made with the maximum expected value of  $R_i$  connected between the input and ground.

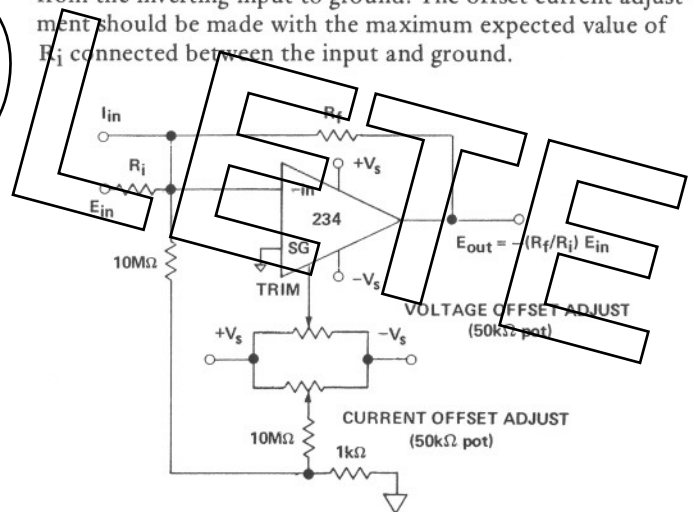


Figure 5. Offset Current Voltage Cancellation

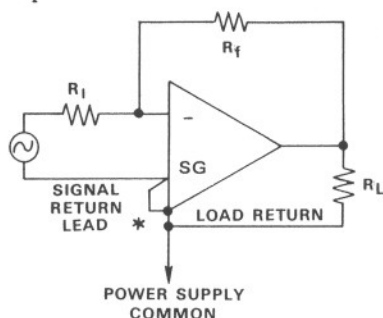
## INVERTING OPERATION

The Model 234 is designed for use in the inverting mode. It is important that the SG (equivalent to +in) terminal be kept at the same potential as the amplifier's "common" terminal. Any voltage difference between these points is similar to a common mode voltage, and performance cannot be guaranteed under such conditions. The Model 234 is also an excellent amplifier for measurement and conversion of low level current sources to proportionate voltages. With offset current externally zeroed, input currents of ten to twenty picoamperes can be amplified and converted to a voltage source for further processing.

## SHIELDING, PICKUP AND GROUNDS

A special feature of the Model 234 is the internal electrostatic shield. This prevents not only pickup of extraneous signals by the module but also prevents radiation of chopper noise by the module. One precaution is to insure that noise sources are shielded from the inverting input. The user should

also insure that ground loops do not occur which can add extraneous signals when amplifying from microvolt or millivolt sources. Figure 6 illustrates the proper connections to avoid ground loops.



\* SIGNAL RETURN AND LOAD RETURN SHOULD BE CONNECTED TO POWER COMMON AS CLOSE TO AMPLIFIER PINS AS POSSIBLE

Figure 6. Ground Connection

### INTERMODULATION CONSIDERATIONS

If noise at medium frequencies (to 400Hz) finds its way into the input circuits of carrier amplifiers (chopper amplifiers and the chopper-stabilizing portions of chopper-stabilized amplifiers), it tends to "beat" with the chopper frequency and produce sum and difference frequencies. The "sum" frequencies are unimportant, because they are usually filtered out; the noise frequency is usually unimportant because it, too, is filtered out. But the difference frequencies (which can include dc) usually interfere directly with the low-level low-frequency signal information.

There are precautions that can be taken by the manufacturer to minimize such interference occurring within the devices themselves; but the user must also be aware of the need for precautions, especially in performing low-level measurements in the presence of:

1. input signals containing high-frequency normal-mode noise components (such as unfiltered carrier from a measuring device)
2. ripple coupled in from power supplies
3. stray electromagnetic radiation at line frequencies, especially if it is rich in harmonics.

This noise may be introduced to the amplifier at either improperly guarded input leads or at the power supply terminals. These effects may be minimized by using shielded supplies which have low ripple and low source impedances at the line harmonics. Properly shielding the input leads, as well as locating the amplifier as far from sources of 60Hz (or 50Hz) magnetic fields, is also recommended for best performance. Mechanical orientation of the amplifier package and layout of signal grounds may also be used to minimize EMI effects.

If a "beat" does occur, it usually manifests itself as a slowly varying offset signal at the output of the amplifier, usually below 20Hz. To examine the extent of this equivalent offset noise voltage in a system, an oscilloscope should be used to monitor the amplifier output with the input signal point shorted to ground. As another test, a low level signal may be applied at the input of the final circuit configuration to determine the intermodulation rejection capability of the design. In this test, the signal frequency should be swept through the modulation frequency point to observe output signal peaking. A low pass output filter, at approximately 40Hz, should be used when making these tests.

### THE "T" NETWORK

High gains and high input impedance to an inverting amplifier normally require excessively large feedback resistors. For ex-

ample, an input impedance of 1,000,000 ohms and a gain of 100 require a feedback resistor of 100 Megohms. Such a resistor is relatively expensive, particularly for low tolerance units. Furthermore, one picofarad of stray capacitance across this single resistor would reduce 3dB bandwidth to 1590Hz, and resistive leakage across PC boards may become a problem. The "T" network in Figure 7 is a means of minimizing these problems. If the ratio  $R_f/R_i$  is at least 5 to 1, there will be no measurable change in other performance characteristics. If the ratio is lower, for instance, 1 to 1, the effective drift and noise gain will be doubled, compared to the signal gain. A general rule is to make the ratio  $R_f/R_i$  approximately equal to the ratio  $R_2/R_1$ . This normally results in reasonable values of resistance for  $R_f$ , and a minimal increase in noise and drift gains compared to the standard two resistor circuit. An additional advantage of the "T" network is variable gain without the necessity of connecting a switch or potentiometer directly to the highly sensitive inverting input terminal. This avoids serious noise pickup problems. In such a hookup,  $R_1$  is the variable element.

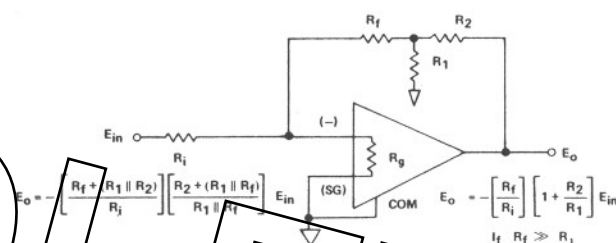


Figure 7 "T" Network

### OVERLOAD RECOVERY

The overload recovery circuit shown in Figure 8 will prevent the input circuitry from becoming saturated. This circuit, connected externally, will allow the amplifier to recover from overload in less than 0.5μsec. Without this circuit overload recovery will require up to 5 seconds.

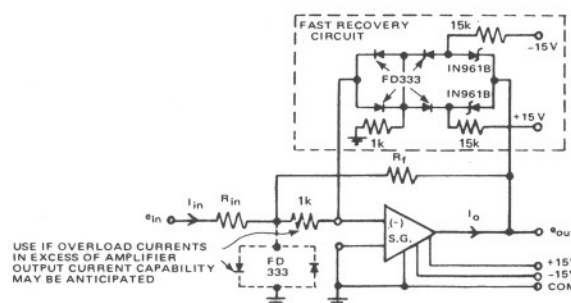


Figure 8. Overload Recovery Circuit

### HIGH SOURCE IMPEDANCE CIRCUITS

When required to operate from source impedances above 100kΩ, the model 234, with inherently lower input current noise and spikes, offers dramatic improvements over previous designs. (See Figure 9)

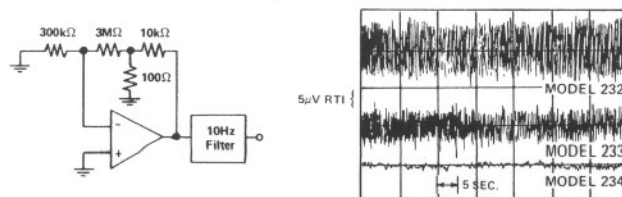


Figure 9. Comparative Input Noise (RTI) Performance in a DC to 10Hz Bandwidth.



# LOW VOLTAGE DRIFT-CHOPPER STABILIZED MODELS 234, 233, 260, 261, 231, 210

## GENERAL DESCRIPTION

Chopper stabilized amplifiers employ modulation techniques for processing the "low frequency" components of a signal and an AC coupled amplifier for the higher frequencies. This chopping technique makes it possible to process wide-band signals and yet achieve superior low drift and long term stability. Analog Devices, a pioneer in the development of encapsulated chopper stabilized amplifiers, offers designs with drifts between  $0.1$  to  $1\mu\text{V}/^\circ\text{C}$ , low frequency voltage noise to  $1\mu\text{V}$  p-p and bias currents from  $50$  to  $300\text{pA}$ . Long term stability averages  $1\mu\text{V}/\text{month}$ . These amplifiers are widely accepted as the best choice when it is essential to maintain either low voltage offsets and bias currents versus time or against severe environmental changes, or whenever external offset adjustments are not possible or desirable.

### MODEL 234 J/K/L: LOWEST NOISE, WIDEBAND

This latest inverting amplifier design from Analog Devices is virtually free of chopper spikes and is singled out as the industry's quietest, wide band chopper stabilized amplifier in a low cost module. To illustrate the significant improvement in performance, comparative noise signals are presented in the figure for model 234 and its predecessor model 232.

Available in three drift selections ( $1$ ,  $0.3$  and  $0.1\mu\text{V}/^\circ\text{C}$ ), model 234 specifications include voltage noise of  $1\mu\text{V}$  p-p, current noise of  $2\text{pA}$  p-p, and  $2.5\text{MHz}$  bandwidth. Slew rate is  $30\text{V}/\mu\text{sec}$ . The wide bandwidth of 234 makes it especially useful for 16-bit D/A converters, high speed integrators as well as for low frequency applications including control systems, DVM input amplifier designs and other precision instrumentation. Attractively priced, its consistent unit-to-unit performance makes it an ideal choice for new OEM designs.

### MODEL 233 J/K/L: LOWEST COST, $0.1\mu\text{V}/^\circ\text{C}$

The popular model 233 is a good choice for many low drift, high gain applications including precision integrators, instrument preamplifiers and null detectors as used to resolve microvolt error signals.

The combination of IC's and improved design techniques in this  $0.4''$  high module results in good performance at low cost for OEM designs.

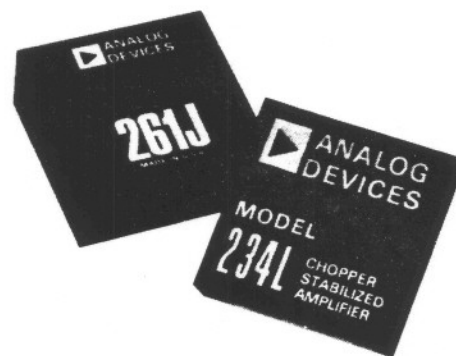
Typical specifications for this inverting amplifier include  $500\text{kHz}$  bandwidth,  $0.25\text{V}/\mu\text{sec}$  slew rate,  $50\text{pA}$  bias current and  $3\mu\text{V}$  p-p noise in a  $10\text{Hz}$  bandwidth. It is available with three drift selections:  $1$ ;  $0.3$ ; and  $0.1\mu\text{V}/^\circ\text{C}$ .

### MODEL 260 J/K: $10^9\Omega$ NONINVERTING, $0.1\mu\text{V}/^\circ\text{C}$

Analog Devices pioneered in the development of new "chopper" amplifier designs to provide high input impedance without compromising the excellent low frequency characteristics of chopper type amplifiers. As embodied in the model 260, this design is useful as a noninverting buffer amplifier for processing microvolt signals with minimal source loading errors. Typical specifications for the model 260 are  $10^9\Omega$  input impedance, drift to  $0.1\mu\text{V}/^\circ\text{C}$  and CMR of  $110\text{dB}$  at  $\pm 1\text{V}$ .

### MODEL 261: GUARANTEED NOISE OF LESS THAN $1\mu\text{V}$

The model 261 is a second generation design which typically provides a significant improvement in the noise and bandwidth characteristics of model 260 and other competitive models.



Model	Lowest Cost General Purpose		
	J	K	L
Open Loop Gain			
DC Rated Load, V/V min			$10^7$
Rated Output, min			$\pm 10\text{V}@5\text{mA}$
Frequency Response			
Unity Gain, Small Signal			$500\text{kHz}$
Full Power Response, min			$4\text{kHz}$
Slewing Rate, min			$0.25\text{V}/\mu\text{s}$
Overload Recovery			—
Input Offset Voltage			
Initial, $25^\circ\text{C}$ (Adj. to zero) max	$\pm 50\mu\text{V}$	$\pm 20\mu\text{V}$	$\pm 20\mu\text{V}$
Avg. vs. Temp ( $0^\circ\text{C}$ to $70^\circ\text{C}$ ) max	$\pm 1.0$	$\pm 0.3$	$\pm 0.1\mu\text{V}/^\circ\text{C}$
vs. Supply Voltage		$\pm 0.2\mu\text{V}/\%$	
vs. Time		$\pm 2\mu\text{V}/\text{mo.}$	
Input Bias Current			
Initial, $25^\circ\text{C}$ , max		$\pm 50\text{pA}$	
Avg. vs. Temp ( $0^\circ\text{C}$ to $70^\circ\text{C}$ ) max	$\pm 2$	$\pm 1$	$\pm 0.5\text{pA}/^\circ\text{C}$
Input Impedance			
Differential			$600\text{k}\Omega$
Common Mode			NA
Input Noise			
Voltage, $0.01$ to $1\text{Hz}$ , p-p			$1\mu\text{V}$
$0.1$ to $10\text{Hz}$ , p-p			$3\mu\text{V}$
$10\text{Hz}$ to $10\text{kHz}$ , rms			$3\mu\text{V}$
Current, $0.01$ to $1\text{Hz}$ , p-p			$3\text{pA}$
$0.1$ to $10\text{Hz}$ , p-p			$6\text{pA}$
Input Voltage Range			
Common Mode Voltage, min			NA
Common Mode Rejection			NA
Max Safe Differential Voltage			$\pm 15\text{V}$
Power Supply Range (VDC)			$\pm (12 \text{ to } 18)\text{V}$
Rated Specification (VDC)			$\pm 15\text{V}@5\text{mA}$
Temperature Range			
Operating, Rated Specifications			$0$ to $+70^\circ\text{C}$
Package Outline			F-3
Case Dimensions			$1.5'' \times 1.5'' \times 0.4''$
Price			
1-9	\$45	\$54	\$75
10-24	\$40	\$49	\$68

(1) Model 260 inverting input bias current  $\pm 3\text{nA}$ , max.

Operating at a higher carrier frequency, this noninverting design features extremely low noise,  $0.4\mu\text{Vp-p}$  in a 1Hz bandwidth; low drift,  $0.1\mu\text{V}/^\circ\text{C}$ ; and an output that is virtually free of chopper spikes.

Model 261 also offers a solution to beat frequency problems caused by a low frequency carrier mixing with harmonics of the AC line. The carrier frequency on this design is nearly a decade higher than that of models previously available, thereby eliminating the possibility of any interaction with the line frequency or its harmonics.

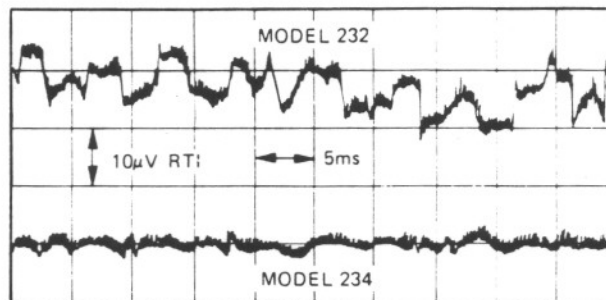
The new model should be considered for all new instruments and circuit applications, or wherever improved performance, at no increase in cost, is desirable for existing sockets. Models 260 and 261 are mechanically and electrically interchangeable for these applications.

Model 261 will be available in production quantities by June of 1973. Evaluation units are available from stock.

#### MODEL 231 J/K: 25mA OUTPUT, $0.1\mu\text{V}/^\circ\text{C}$

Model 231, available in two drift selections (231J,  $0.25\mu\text{V}/^\circ\text{C}$  and 231K,  $0.1\mu\text{V}/^\circ\text{C}$ ) is an inverting chopper stabilized amplifier with increased output current capability (25mA). With stable 3kHz full power response and low drift, it offers higher output without use of an additional booster stage for heavier load requirements.

**MODELS 210/211:  $100\text{V}/\mu\text{sec}$  WIDEBAND,  $1\mu\text{V}/^\circ\text{C}$**   
Models 210/211 with 20mA output, are inverting chopper stabilized amplifiers for that class of application requiring low drift performance with good high frequency performance. This design will provide slew rates of  $100\text{V}/\mu\text{sec}$  and 90dB of loop gain at 10kHz for improved wideband accuracy. Incorporating internal limiting circuitry, these amplifiers have exceptionally fast overload recovery, (0.2 $\mu\text{sec}$ ) and stable input characteristics for high speed integrator and comparator designs. They are available in two drift selections (model 210,  $1\mu\text{V}/^\circ\text{C}$ , model 211,  $2\mu\text{V}/^\circ\text{C}$ ).



DC to 1kHz Noise, Referred to the Input; 234 vs 232.

High Performance Wideband 1 $\mu\text{V}$ p-p Lowest Noise 234			Low Cost Non-Inverting High $Z_{in}$ 260		General Purpose 25mA Output 231		High Bandwidth 20mA Output 210/211	
J	K	L	J	K	J	K	210	211
$10^7$			$5 \times 10^6$		$10^7$		$10^8$	
$\pm 10\text{V}@5\text{mA}$			$\pm 10\text{V}@5\text{mA}$		$\pm 10\text{V}@25\text{mA}$		$\pm 10\text{V}@20\text{mA}$	
2.5MHz 500kHz 30V/ $\mu\text{s}$ —			100Hz 2 to 50Hz 100V/s 30ms		500kHz 3kHz 0.2V/ $\mu\text{s}$ 3.0sec		20MHz 500kHz 100V/ $\mu\text{s}$ 0.2 $\mu\text{s}$	
$\pm 50\mu\text{V}$ $\pm 1.0$	$\pm 25\mu\text{V}$ $\pm 0.3$	$\pm 25\mu\text{V}$ $\pm 0.1\mu\text{V}/^\circ\text{C}$	$\pm 25\mu\text{V}$ $\pm 0.1\mu\text{V}/^\circ\text{C}$ $\pm 0.1\mu\text{V}/\%$ $\pm 1.0\mu\text{V}/\text{mo.}$		$\pm 15\mu\text{V}$ $\pm 0.25$ $\pm 0.1\mu\text{V}/\%$ $\pm 1.0\mu\text{V}/\text{mo.}$		$\pm 100\mu\text{V}$ $\pm 0.5$ $\pm 1\mu\text{V}/^\circ\text{C}$ $\pm 10\mu\text{V}/\%$ $\pm 1.0\mu\text{V}/\text{day}$	
$\pm 4$	$\pm 100\text{pA}$ $\pm 2$	$\pm 2\text{pA}/^\circ\text{C}$	$\pm 300\text{pA}^1$ $\pm 10\text{pA}/^\circ\text{C}$		$\pm 100\text{pA}$ $\pm 1.0$ $\pm 50\text{pA}$ $\pm 0.5\text{pA}/^\circ\text{C}$		$\pm 100\text{pA}$ $\pm 1$ $\pm 150\text{pA}$ $\pm 3\text{pA}/^\circ\text{C}$	
300k $\Omega$ NA			80k $\Omega$ //0.01 $\mu\text{F}$ 10 $^9\Omega$ //0.02 $\mu\text{F}$		300k $\Omega$ NA		500k $\Omega$ NA	
0.7 $\mu\text{V}$ 1.5 $\mu\text{V}$ 2 $\mu\text{V}$ 2pA 4pA			0.4 $\mu\text{V}$ 1.0 $\mu\text{V}$ — 4pA 10pA		1.5 $\mu\text{V}$ 10 $\mu\text{V}$ 5 $\mu\text{V}$ 10pA 35pA		5 $\mu\text{V}$ — 10 $\mu\text{V}$ 10pA —	
NA NA $\pm 15\text{V}$			$\pm 1.0\text{V}$ 110dB $\pm 20\text{V}$		NA NA $\pm 15\text{V}$		NA NA $\pm 15\text{V}$	
$\pm(12 \text{ to } 18)\text{V}$ $\pm 15\text{V}@5\text{mA}$			$\pm(10 \text{ to } 18)\text{V}$ $\pm 15\text{V}@6\text{mA}$		$\pm(12 \text{ to } 18)\text{V}$ $\pm 15\text{V}@+8, -10\text{mA}$		$\pm(12 \text{ to } 18)\text{V}$ $\pm 15\text{V}@+30, -4\text{mA}$	
0 to $+70^\circ\text{C}$ F-3			0 to $+70^\circ\text{C}$ FA-6		0 to $+70^\circ\text{C}$ WA-1		0 to $+70^\circ\text{C}$ R-7	
1.5" x 1.5" x 0.4"			1.5" x 1.5" x 0.62"		3.6" x 1.6" x 0.4"		2.87" x 1.37" x 0.99"	
\$54	\$65	\$89	\$49	\$64	\$80	\$115	\$157	\$113
\$49	\$59	\$82	\$45	\$58	\$74	\$105	\$148	\$107

# LOW VOLTAGE DRIFT-CHOPPER STABILIZED MODELS 234, 233, 260, 261, 231, 210

## GENERAL DESCRIPTION

Chopper stabilized amplifiers employ modulation techniques for processing the "low frequency" components of a signal and an AC coupled amplifier for the higher frequencies. This chopping technique makes it possible to process wide-band signals and yet achieve superior low drift and long term stability. Analog Devices, a pioneer in the development of encapsulated chopper stabilized amplifiers, offers designs with drifts between 0.1 to  $1\mu\text{V}/^\circ\text{C}$ , low frequency voltage noise to  $1\mu\text{V}$  p-p and bias currents from 50 to 300pA. Long term stability averages  $1\mu\text{V}/\text{month}$ . These amplifiers are widely accepted as the best choice when it is essential to maintain either low voltage offsets and bias currents versus time or against severe environmental changes, or whenever external offset adjustments are not possible or desirable.

## MODEL 234 J/K/L: LOWEST NOISE, WIDEBAND

This latest inverting amplifier design from Analog Devices is virtually free of chopper spikes and is singled out as the industry's quietest, wide band chopper stabilized amplifier in a low cost module. To illustrate the significant improvement in performance, comparative noise signals are presented in the figure for model 234 and its predecessor model 232.

Available in three drift selections (1, 0.3 and  $0.1\mu\text{V}/^\circ\text{C}$ ), model 234 specifications include voltage noise of  $1\mu\text{V}$  p-p, current noise of 2pA p-p, and 2.5MHz bandwidth. Slew rate is  $30\text{V}/\mu\text{sec}$ . The wide bandwidth of 234 makes it especially useful for 16-bit D/A converters, high speed integrators as well as for low frequency applications including control systems, DVM input amplifier designs and other precision instrumentation. Attractively priced, its consistent unit-to-unit performance makes it an ideal choice for new OEM designs.

## MODEL 233 J/K/L: LOWEST COST, $0.1\mu\text{V}/^\circ\text{C}$

The popular model 233 is a good choice for many low drift, high gain applications including precision integrators, instrument preamplifiers and null detectors as used to resolve microvolt error signals.

The combination of IC's and improved design techniques in this 0.4" high module results in good performance at low cost for OEM designs.

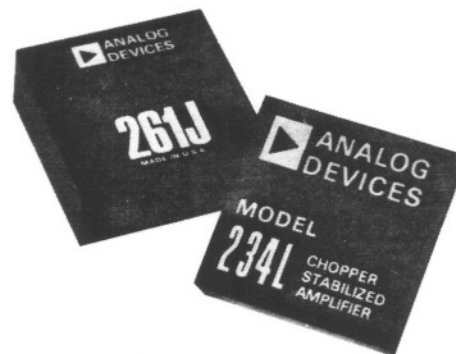
Typical specifications for this inverting amplifier include 500kHz bandwidth,  $0.25\text{V}/\mu\text{sec}$  slew rate, 50pA bias current and  $3\mu\text{V}$  p-p noise in a 10Hz bandwidth. It is available with three drift selections: 1; 0.3; and  $0.1\mu\text{V}/^\circ\text{C}$ .

## MODEL 260 J/K: $10^9\Omega$ NONINVERTING, $0.1\mu\text{V}/^\circ\text{C}$

Analog Devices pioneered in the development of new "chopper" amplifier designs to provide high input impedance without compromising the excellent low frequency characteristics of chopper type amplifiers. As embodied in the model 260, this design is useful as a noninverting buffer amplifier for processing microvolt signals with minimal source loading errors. Typical specifications for the model 260 are  $10^9\Omega$  input impedance, drift to  $0.1\mu\text{V}/^\circ\text{C}$  and CMR of 110dB at  $\pm 1\text{V}$ .

## MODEL 261: GUARANTEED NOISE OF LESS THAN $1\mu\text{V}$

The model 261 is a second generation design which typically provides a significant improvement in the noise and bandwidth characteristics of model 260 and other competitive models.



Model	Lowest Cost General Purpose		
	J	K	L
Open Loop Gain			
DC Rated Load, V/V min		$10^7$	
Rated Output, min		$\pm 10\text{V}@5\text{mA}$	
Frequency Response			
Unity Gain, Small Signal		500kHz	
Full Power Response, min		4kHz	
Slewing Rate, min		$0.25\text{V}/\mu\text{s}$	
Overload Recovery		—	
Input Offset Voltage			
Initial, $25^\circ\text{C}$ (Adj. to zero) max	$\pm 50\mu\text{V}$	$\pm 20\mu\text{V}$	$\pm 20\mu\text{V}$
Avg. vs. Temp ( $0^\circ\text{C}$ to $70^\circ\text{C}$ ) max	$\pm 1.0$	$\pm 0.3$	$\pm 0.1\mu\text{V}/^\circ\text{C}$
vs. Supply Voltage		$\pm 0.2\mu\text{V}/\%$	
vs. Time		$\pm 2\mu\text{V}/\text{mo.}$	
Input Bias Current			
Initial, $25^\circ\text{C}$ , max		$\pm 50\text{pA}$	
Avg. vs. Temp ( $0^\circ\text{C}$ to $70^\circ\text{C}$ ) max	$\pm 2$	$\pm 1$	$\pm 0.5\text{pA}/^\circ\text{C}$
Input Impedance			
Differential		$600\text{k}\Omega$	
Common Mode		NA	
Input Noise			
Voltage, 0.01 to 1Hz, p-p		$1\mu\text{V}$	
0.1 to 10Hz, p-p		$3\mu\text{V}$	
10Hz to 10kHz, rms		$3\mu\text{V}$	
Current, 0.01 to 1Hz, p-p		3pA	
0.1 to 10Hz, p-p		6pA	
Input Voltage Range			
Common Mode Voltage, min		NA	
Common Mode Rejection		NA	
Max Safe Differential Voltage		$\pm 15\text{V}$	
Power Supply Range (VDC)		$\pm (12 \text{ to } 18)\text{V}$	
Rated Specification (VDC)		$\pm 15\text{V}@5\text{mA}$	
Temperature Range			
Operating, Rated Specifications		0 to $+70^\circ\text{C}$	
Package Outline		F-3	
Case Dimensions		1.5" x 1.5" x 0.4"	
Price			
1-9	\$45	\$54	\$75
10-24	\$40	\$49	\$68

(1) Model 260 inverting input bias current  $\pm 3\text{nA}$ , max.

Operating at a higher carrier frequency, this noninverting design features extremely low noise,  $0.4\mu\text{Vp-p}$  in a 1Hz bandwidth; low drift,  $0.1\mu\text{V}/^\circ\text{C}$ ; and an output that is virtually free of chopper spikes.

Model 261 also offers a solution to beat frequency problems caused by a low frequency carrier mixing with harmonics of the AC line. The carrier frequency on this design is nearly a decade higher than that of models previously available, thereby eliminating the possibility of any interaction with the line frequency or its harmonics.

The new model should be considered for all new instruments and circuit applications, or wherever improved performance, at no increase in cost, is desirable for existing sockets. Models 260 and 261 are mechanically and electrically interchangeable for these applications.

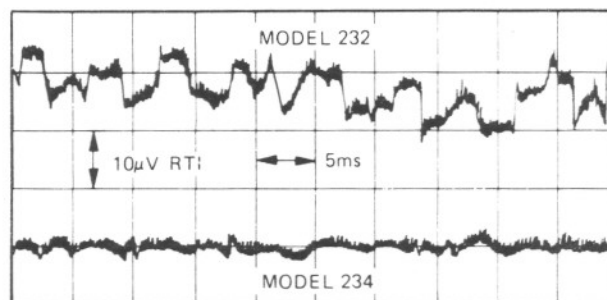
Model 261 will be available in production quantities by June of 1973. Evaluation units are available from stock.

#### MODEL 231 J/K: 25mA OUTPUT, $0.1\mu\text{V}/^\circ\text{C}$

Model 231, available in two drift selections (231J,  $0.25\mu\text{V}/^\circ\text{C}$  and 231K,  $0.1\mu\text{V}/^\circ\text{C}$ ) is an inverting chopper stabilized amplifier with increased output current capability (25mA). With stable 3kHz full power response and low drift, it offers higher output without use of an additional booster stage for heavier load requirements.

#### MODELS 210/211: $100\text{V}/\mu\text{sec}$ WIDEBAND, $1\mu\text{V}/^\circ\text{C}$

Models 210/211 with 20mA output, are inverting chopper stabilized amplifiers for that class of application requiring low drift performance with good high frequency performance. This design will provide slew rates of  $100\text{V}/\mu\text{sec}$  and 90dB of loop gain at 10kHz for improved wideband accuracy. Incorporating internal limiting circuitry, these amplifiers have exceptionally fast overload recovery, (0.2 $\mu\text{sec}$ ) and stable input characteristics for high speed integrator and comparator designs. They are available in two drift selections (model 210,  $1\mu\text{V}/^\circ\text{C}$ , model 211,  $2\mu\text{V}/^\circ\text{C}$ ).

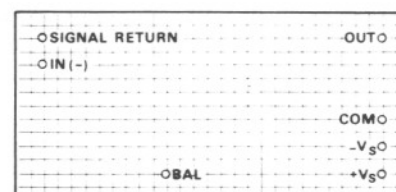


DC to 1kHz Noise, Referred to the Input; 234 vs 232.

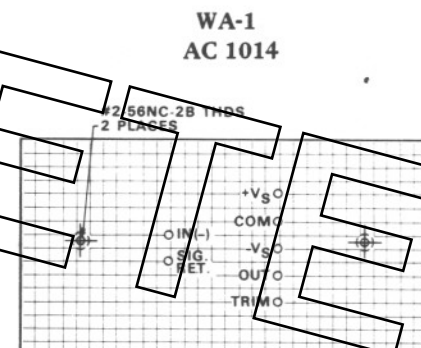
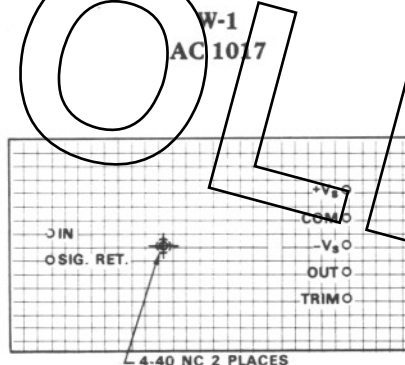
High Performance Wideband $1\mu\text{V p-p}$ Lowest Noise 234			Low Cost Non-Inverting High $Z_{IN}$ 260		General Purpose 25mA Output 261		High Bandwidth 20mA Output 210/211	
J	K	L	J	K	J	K	210	211
$10^7$			$5 \times 10^6$		$10^7$		$10^8$	
$\pm 10\text{V}@5\text{mA}$			$\pm 10\text{V}@5\text{mA}$		$\pm 10\text{V}@25\text{mA}$		$\pm 10\text{V}@20\text{mA}$	
2.5MHz 500kHz 30V/ $\mu\text{s}$ —			100Hz 2 to 50Hz 100V/s 30ms		500kHz 3kHz 0.2V/ $\mu\text{s}$ 3.0sec		20MHz 500kHz 100V/ $\mu\text{s}$ 0.2 $\mu\text{s}$	
$\pm 50\mu\text{V}$ $\pm 1.0$	$\pm 25\mu\text{V}$ $\pm 0.3$ $\pm 0.2\mu\text{V}/\%$ $\pm 2\mu\text{V}/\text{mo.}$	$\pm 25\mu\text{V}$ $\pm 0.1\mu\text{V}/^\circ\text{C}$	$\pm 0.3$ $\pm 0.1\mu\text{V}/\%$ $\pm 0.1\mu\text{V}/^\circ\text{C}$ $\pm 1.0\mu\text{V}/\text{mo.}$		$\pm 0.25$ $\pm 0.1\mu\text{V}/\%$ $\pm 0.1\mu\text{V}/^\circ\text{C}$ $\pm 1.0\mu\text{V}/\text{mo.}$		$\pm 0.5$ $\pm 100\mu\text{V}$ $\pm 10\mu\text{V}/\%$ $\pm 1\mu\text{V}/^\circ\text{C}$ $\pm 1.0\mu\text{V}/\text{day}$	
$\pm 4$	$\pm 100\text{pA}$ $\pm 2$	$\pm 2\text{pA}/^\circ\text{C}$	$\pm 300\text{pA}^1$ $\pm 10\text{pA}/^\circ\text{C}$		$\pm 100\text{pA}$ $\pm 1.0$ $\pm 50\text{pA}$ $\pm 0.5\text{pA}/^\circ\text{C}$		$\pm 100\text{pA}$ $\pm 1$ $\pm 150\text{pA}$ $\pm 3\text{pA}/^\circ\text{C}$	
300k $\Omega$ NA			80k $\Omega$ //0.01 $\mu\text{F}$ 10 $^9\Omega$ //0.02 $\mu\text{F}$		300k $\Omega$ NA		500k $\Omega$ NA	
0.7 $\mu\text{V}$ 1.5 $\mu\text{V}$ 2 $\mu\text{V}$ 2pA 4pA			0.4 $\mu\text{V}$ 1.0 $\mu\text{V}$ — 4pA 10pA		1.5 $\mu\text{V}$ 10 $\mu\text{V}$ 5 $\mu\text{V}$ 10pA 35pA		5 $\mu\text{V}$ — 10 $\mu\text{V}$ 10pA —	
NA NA $\pm 15\text{V}$			$\pm 1.0\text{V}$ 110dB $\pm 20\text{V}$		NA NA $\pm 15\text{V}$		NA NA $\pm 15\text{V}$	
$\pm(12 \text{ to } 18)\text{V}$ $\pm 15\text{V}@5\text{mA}$			$\pm(10 \text{ to } 18)\text{V}$ $\pm 15\text{V}@6\text{mA}$		$\pm(12 \text{ to } 18)\text{V}$ $\pm 15\text{V}@+8, -10\text{mA}$		$\pm(12 \text{ to } 18)\text{V}$ $\pm 15\text{V}@+30, -4\text{mA}$	
0 to $+70^\circ\text{C}$ F-3 1.5" x 1.5" x 0.4"			0 to $+70^\circ\text{C}$ FA-6 1.5" x 1.5" x 0.62"		0 to $+70^\circ\text{C}$ WA-1 3.6" x 1.6" x 0.4"		0 to $+70^\circ\text{C}$ R-7 2.87" x 1.37" x 0.99"	
\$54 \$49	\$65 \$59	\$89 \$82	\$49 \$45	\$64 \$58	\$80 \$74	\$115 \$105	\$157 \$148	\$113 \$107



## MODELS 210, 211



W, WA PACKAGES  
MODELS 231, 310, 311



The mechanical drawing shows the physical dimensions of the Model 6000 module. The top view indicates a width of 3.2 units and a height of 3.3 units. It features four potentiometers labeled GAIN ADJUST (R<sub>4</sub>), OFFSET (R<sub>1</sub>), X ZERO (R<sub>3</sub>), and Y ZERO (R<sub>2</sub>). A central rectangular area is labeled MODULE. The bottom edge has connection points for +V<sub>S</sub>, -COM, COM, -V<sub>S</sub>, OUT, X IN, and Y IN. The side view shows a total depth of 1.072 units, with a .84 unit section at the top and a .16 unit section below it. A 0.31 unit dimension is shown at the bottom right corner.

1. Model 425 gain adjust pot in series with X input.
2. Mating socket supplied with unit (ADI part no. 60-42820).